ヘリウム損傷ナノ構造形成タングステンの冷却特性と損傷回避法

Cooling Characteristics and Mitigation of He-Defected Tungsten with Nanostructured Surface

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Abstract Precise evaluation of radiation cooling capability of the tungsten with fiber-form nanostructure is done using an electron beam power calibration system. It is found that the total emissivity of black nanostructured tungsten is very close to 1.0, meaning a complete black body. Discrepancies for the determination of total emissivity between the electron beam method and the fixed biasing procedure were discussed in terms of energy transmission through the plasma sheath, focusing on the ion energy reflection and the cooling associated by secondary electron emission. Some recovery techniques to obtain an almost original flat tungsten surface from nanostructured one is introduced, emphasizing on ITER-grade tungsten. Finally the effect of thin carbon layer on the formation of nanostructure on the tungsten surface is demonstrated as a mitigation technique.

1. Introduction

Tungsten (W) material is very important in terms of plasma-facing component not only in DEMO but also in ITER. But helium (He) radiation defects are strong concerns when employing W for the divertor target and/or the first wall because of an enormous heat load on such plasma-facing tungsten surfaces. Here, we note that He is one of fusion products. The fiber-form nanostructure, so called "fuzz", has been investigated on a variety of W surface irradiated by He or He/D mixture plasmas since it was recently found ^{1, 2)}. In Alcator C-Mod with all metal wall (Mo and W) it has been really observed at the outer strike point ³⁾.

Cooling capability of nanostructured W is a curious issue, especially against big transient heat loads like ELMs. It is very important to mention that the enhanced power radiation due to an increased emissivity may contribute in particular for big ELM heat pulses because the radiated power amounts to a few tens percents of the steady state power load of about 10 MW/m². A quantitative evaluation of cooling characteristics can be obtained by determining the total emissivity (TE) e_t through the power balance equation using Stefan-Boltzmann law, $P = e_t \sigma T^4 S$ where P is the power input to the target, σ is the Stefan-Boltzmann constant, T is the surface temperature, and S is the surface area.

Although we have some favorable properties of the tungsten with fiber-form nanostructure on its surface ^{4, 5)}, such as enhanced cooling ⁶⁾, suppression of secondary electron emission (SEE) ⁷⁾, and some resistance against cracking ^{8, 9)}, the possibilities of dust formation and arcing ^{10, 11)} would be serious issues so that some recovery ¹²⁾ or mitigation technique will be welcome.

In this research work, some tries to determine the TE by the temperature change are introduced, while the calibration using an electron beam power are compared to the above estimations with a discussion about the plasma power incidence on the target material. Then, some recovery processes will be shown as well as a mitigation technique with a thin film formation on W surface.

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2. Evaluation of Total Emissivity

The TE is the most appropriate measure for the radiation cooling characteristics. It is well documented for normal W $^{13)}$, and has been confirmed by an electron beam calibration $^{14)}$. However, we do not have enough evaluations of those for nanostructured W $^{15, 16)}$. The experiment has been done in the compact plasma device AIT-PID $^{17)}$.

2.1 Fixed Biasing Method

We try to estimate the TE by a change in surface temperature on the way to nanostructure formation. The Stefan-Boltzmann law is invoked by assuming that the fixed biasing of the target does not change the plasma heat flux substantially and that the conduction loss through the thin sheath of the R-type thermocouple with the diameter of 0.5 mm can be almost negligible in such a high temperature range. Figure 1 shows the time evolutions of W temperature in the He plasma with a fixed biasing of -90 V with respect to the potential of vacuum chamber of AIT-PID together with the photo showing an assembly of the W target and the thermocouple, where the plasma potential is + 5 V. The TE obtained with the relation of $e_t^*(t)\sigma\{T^*(t)\}^4S = e_t$ σT^4S ,where the right-hand side corresponds to the virgin W at the start with $e_t = 0.18$ at this temperature ¹³. A substantial increase in the TE has been observed. The final value is about 0.54 in the present case. Several similar experiments gave it over the range between 0.45 and 0.55. Here, we assume that the macroscopically geometric surface area does not change with the nanostructure formation. But the microscopic area is effectively increased. However, we do not need to know the exact microscopic surface area because this increase is converted to the radiation emissivity with a constant surface area.

A similar but different approach is shown in Fig.2 where W with nanostructure was exposed to Ar plasma in AIT-PID which provided a sputtering of W surface leading to a normal flat W with a biasing of - 100 V. The starting and final biasing voltages are the same, - 12V, in between the biasing voltage is set down to - 100 V in order to enhance the sputtering. The TE at the final stage $e_t = 0.14$ for the temperature of 1150 K. It is traced back to the original nanostructured tungsten. Again the value for the TE is close to 0.50.



Fig. 1 Time evolutions of the temperature of PM-W $(10 \times 10 \times 1 \text{ mm}^3)$ measured with R-type thermocouple (0.5 mm in diameter) and the corresponding apparent total emissivity deduced Stefan-Boltzmann law on the way to nanostructure formation in He plasma with a fixed biasing voltage.



Fig. 2 Temporal changes in PM-W temperature measured with thermocouple, biasing current, biasing voltage and calculated apparent total emissivity in the sputtering process in Ar plasma for the originally nanostructured W.

2.2 Electron Beam Method

The absolute value of TE has been estimated by a completely different way from the previous method, using the known electron beam power for the same tungsten target in which the thermocouple is inserted. The device for the present purpose is almost the same as AIT-PID as shown in Fig.3(a) under the vacuum condition without any gas feeding, but a small grounded molybdenum mesh (20 meshes/inch) just in front of LaB₆ cathode is set at the head of boron-nitride (BN) hood as shown in Fig.3(b) to pull out the electrons by the voltage of V_1 along the axis of vacuum chamber where the multicusp magnetic field intensity is very weak or zero. The electron beam is transported through this region to arrive the W target which is positively biased by V_2 with respect to the grounded chamber,

while the cathode is negatively biased to have an acceleration of electrons. Such a potential configuration may inhibit any release of secondary electrons from the target which ensures that the input power to the target can be calculated by the product of the target current and the acceleration voltage which corresponds to $V_1 + V_2$.



Fig. 3 Schematic diagram of electron beam calibration system using AIT-PID (a) and electron beam source (b).

The relations between the target input power and the temperature are shown in Fig.4 for the virgin as well as nanostructured black W with the size of 15x15x1 mm³. In the case of the black W with fiber-form nanostructure on its surface, a fairly rapid measurement ensures а negligible change in nanostructure coming from a kind of annealing although the maximum temperature is less than 1200 K which is much lower than the temperature for annealing ^{12, 18)}, e.g. more than 1600 K. Such a careful measurement makes the number of data points not so large as those for virgin W. Some small corrections are made for the power balance equation: $P = e_t(T)\sigma ST^4 +$ $\kappa T - P_0$ where P_0 is the additional power input from LaB₆ heat radiation and the second term corresponds to the conduction loss through the metallic sheath of thermocouple. The data points are well reproduced by the fitted curves. The corrections the Stephan-Boltzmann relation, $\kappa T - P_0$, are less than 10 % at $T \sim 1000$ K. The value of κ is 2.0 x 10^{-3} W/K

and P_0 is 2W for virgin W and 3 W for nanostructured W. The temperature dependence formula of total emissivity for virgin W shown in the figure comes from the reference ¹³⁾. We note that more than 400 K temperature reductions are detected, which is larger than the temperature changes shown in Figs. 1 and 2. The electron beam calibration gives the TE close to 1.0 corresponding to almost black body for nanostructured W.



Fig. 4 Relation between the temperature T and the input power P for virgin tungsten as well as blackened one with the nanostructure, obtained with the electron beam calibration system.

2.3 Discussions on the Difference in Total Emissivity

We have to examine the discrepancy between the above two methods to determine the TE. The fixed biasing method assumes that under the fixed biasing the plasma gives the same power input to the target even on the way to surface modification. A schematic view for the power into the target due to ions and electrons is shown in Fig.5 where R_{iE} is the ion energy reflection coefficient on the tungsten surface and ϕ_w is the tungsten work function. Therefore, 1 - R_{iE} is the fraction of ion kinetic energy given to the surface. If the ion energy reflection coefficient on both samples is commonly zero or equal and there is no SEE, then we are certain that the power inputs are the same for both kinds of tungsten. However, the ion energy reflection coefficient would be different between these two which have different surface morphologies. Recently, it was found that the nanostructured W gives a smaller ion energy reflection coefficient compared with the flat tungsten without nanostructure ¹⁹⁾. In addition we have energetic electrons which may generate SEE ¹⁷⁾. Secondary electrons may come out to the surface from the metallic bulk by consumption of the energy

corresponding to the work function, ~4.54 eV in the present case. As mentioned above, deep troughs produced by fiber-form nanostructure makes the incident ion kinetic energy to be consumed much more by multi-collisions with nano-fibers compared with a simple reflection from the flat normal surface. According to the suppression of SEE, we can say that the nanostructured W gets more plasma heat power than the flat normal W does under the same biasing condition. We may write $P_v = e_{tv} \sigma T_v^4 S$ for virgin W and $P_B = e_{tB} \sigma T_B^4 S$ for the final stage of nanostructure formation in Fig.1 by neglecting a small heat conduction loss. The relation, $e_{tB} = e_{tv}(T_v/T_B)^4(P_B/T_B)^4$ P_{v}), is derived. For the case that $P_{B} > P_{v}$ as discussed above, then we must say an underestimation of TE for the fixed biasing method. It means that the plasma heat loads P_v and P_B must be determined precisely by taking account of various surface effects, like ion energy reflection, SEE, and so on. Therefore, it is recognized that the sheath voltage dependence of power transmission factor is very important, especially those for nanostructured as well as virgin W surface in plasmas with high energy electron component.

Plasma



Fig. 5 Schematic diagram showing the energy input and output mechanisms at the target due to plasma ion and electron incidences. R_{iE} is the ion energy reflection coefficient and ϕ_w is the work function.

3. Recovery and Mitigation

3.1. Dust Formation

One of the serious issues for the W with the fiber-form nanostructure is a dust formation. It seems that so called "fuzz" may easily peel off due to a mechanical or a thermal shock. In fact an adhesive carbon tape on the defected W sticks the nanostructure easily as shown in Fig.6(a). Instead these structures can be shaved also easily with a cutting knife. A shaved

surface is shown in Fig.6(b) where many holes can be seen over all the shaved area, and a remain of nanostructure can be seen at the edge of upper right. The dust thus collected is also shown in Fig.6(c) and (d). A kind of fragility has been demonstrated in these treatments.



Fig. 6 Possibility of W dust formation from nanostructured W. (a) Nano-fibers peeled off from it on an adhesive carbon tape, (b) shaved W surface with cutting knife, (c) collected W nano-fibers and (d) the magnified view.

3.2. Recovery

If we can develop a recovery technique from defected W to normal W, it could be beneficial. With respect to recovery towards the normal flat surface, preferably without any bubbles inside, the argon plasma annealing technique has been employed, in which the W surface temperature was elevated up to around 1850 K by making the target potential towards the plasma potential for the exposure time of 25 min ¹⁸⁾. The plasma heat comes mainly from electrons, while the ion energy is too low to have a sputtering. This idea was based on the effect of temperature excursion on the W surface morphology, that is, shrinkage and fattening of W fibers on the surface ⁶⁾. The technique has been extended to the case of He plasma annealing with the surface temperature of 1800 K for 60 min by the electronic heat load with a small sheath voltage less than 6 V in order to avoid additional formation of bubbles/holes 12, 20).

Figure 7 shows time evolutions of the biasing voltage and the surface temperature over the recovery process



Fig. 7 Temporal evolutions of the biasing voltage and the surface temperature measured with IR-thermometer for ITER-grade W with fiber-form nanostructure originally on its surface on the way to recovery of the surface.

for the ITER-grade W which has the same production procedure as for PM-W (Powder Metallurgy Tungsten), but the plasma-facing surface is perpendicular to the compressed layers. A spontaneous increase in surface temperature at the beginning with a fixed biasing voltage comes from the reduction in the total emissivity of W surface due to plasma annealing. After sufficient plasma annealing, we have a steady temperature.

8 shows surface morphologies Figure of ITER-grade W observed with FE-SEM, where (a) shows a virgin surface as well as a photo of whole target. We can distinguish many parallel lines on the surface coming from pressed layers. Figure 8(b) shows surface morphology made а of fiber-form nanostructure, and a photo of the black target. A recovery is shown in Figs.8(c) and (d) with different magnifications together with a photo of a silver-colored recovered W target. We can distinguish some tiny holes although an apparent flat surface has been recovered.

Figure 9 shows some examples of recovered surfaces as well as original fiber-form nanostructured surface. Recovered surface for PM-W is shown in Fig.9(b), and advanced W material TFGR-W 1.1%TiC/H (Toughing, Fine-Grained Recrystalized W with TiC dispersoid) ²¹⁾ is also shown in Fig.9(c), obtained by the same plasma annealing condition as for PM-W. The recovery for TFGR-W is somewhat incomplete ¹²⁾. Concerning ITER-grade W, it has a recovery property similar to the normal PM-W. The recovered ITER-grade W has also similar bubbles with 50 ~ 100 nm in diameter under about 100 nm in depth.



Fig. 8 FE-SEM images for ITER-grade tungsten. (a) Virgin surface. The photo is inserted. (b) Nanostructure formed on the target (a) with the photo of black target. (c) and (d) Recovered surfaces which contains some holes on its surface. The photo is inserted.



Fig. 9 Original fiber-form nanostructured and plasma annealed W surfaces. (a) Nanostructure of He-defected PM-W due to He plasma irradiation where (a-1) shows a top surface and (a-2) is its cross-section. (b) recovered structure of PM-W where (b-1) is the top surface and (b-2) grazing view, and (c-1) and (c-2) are recovered top views for TFGR-W with different magnifications.

3.3. Mitigation

The most effective way against the formation of nanostructure on the W surface is to suppress the formation process itself. One way for the suppression is to make a thin carbon layer on the tungsten surface which prevents the helium ions to arrive at the tungsten. The thickness of carbon layer must be sufficiently large compared with the penetration depth of helium ions which is a few tens nanometer at most. The physical sputtering of carbon with He ion bombardment may dissipate the carbon layer. For example, the sputtering yield for 100 eV He is about 0.03. In addition, the chemical sputtering due to hydrogen ions may increase the erosion of carbon layer. Here, we try to demonstrate the principle of mitigation with carbon thin film. Figure 10 shows the schematic drawing of the system producing the carbon film formation on the W target with an introduction of methane gas into He plasmas.

The best condition has been looked for by changing the CH₄ gas flow rate and deposition time in helium – methane mixed gas discharge as shown in Table 1. The standard operation condition for the carbon film deposition is as follows: the He gas flow rate: 70 sccm, the CH₄ gas flow rate: 0.5 sccm, the discharge current $I_d = 7.5$ A and the deposition time is 60 min. The starting surface temperature is about 1240 ~ 1280 K, but the final temperature decreases down to 990 ~ 940 K due to radiation cooling caused by an increase in radiation emissivity.



Fig. 10 Schematic drawing of the system producing thin carbon film formation on the W target with an introduction of methane gas.

Figure 11 shows the cross-section of carbon layer on the thin (35 µm) W plate. The thickness of 500 nm carbon film was found to be formed under the above mentioned standard operation. The carbon coated thick W target with R-type thermocouple (0.5 mm ϕ) was exposed to a pure He plasma with the discharge current of I_d = 15 A, He gas flow rate of 70 sccm and the biasing voltage of -40 V (the ion incident energy: 45 eV), which is a typical He plasma condition producing a fiber-form nanostructure for virgin W without carbon layer. The typical temperature history measured with R-type thermocouple is shown in Fig.12, showing the temperature of 1120 to 1180 K. We confirmed no nanostructure formation on this sample as shown by the SEM photo inserted in Fig.12.

Table 1 Experimental conditions for the formation of protective carbon film against the fiber-form nanostructure growth on W surface.

Carbon Film Formation He: 70 secm: Vbias = -15V					
[seem]		[min]	[mm]		
0.4	5.0	30	0.1	_	× *
0.5	7.5	60	1.0	1280(ε=0.43)→940(ε=1.0)	○ **
He Plasma Exposure					
He: 70 sccm; Id = 15 A; V _{bias} = -40 V					
*T = 1060 \sim 1160 K (ϵ = 1.0 IR Thermometer);					
$**T = 1120 \sim 1180 \text{ K} (\text{Thermocouple})$					



Fig. 11 FE-SEM photo showing the cross-section of W substrate deposited by carbon layer under the standard condition.

In order to demonstrate more clearly, the following procedure has been employed. First, a W sample of $10 \times 10 \times 0.1 \text{ mm}^3$ was covered with another

thin W in a reduced size of $10 \times 7 \times 0.035$ mm³. This double W sample was exposed to He (70 sccm) and methane(0.5 sccm) mixed gas discharge plasma with the discharge current of 7.5 A and the target biasing of -15 V for one hour to have a carbon film coating on the whole surface.



Fig. 12 Pure He plasma exposure on carbon coated tungsten prepared with the standard carbon deposition condition. Insertion shows the FE-SEM photo showing no nanostructure formation after pure He plasma exposure for two hours.

Then, the thin cover W is removed to have a fresh W area. The sample with two areas was exposed to pure He plasma with a biasing voltage of -40 V for two hours with the surface temperature of 1100 K. The macroscopic view for the sample after He plasma exposure is shown in Fig.13 where the black area has a nanostructure while the gray one does not.



Fig. 13 Photo of W surface where two areas of fiber-form nanostructure are developed, black one with fiber-form nanostructure and gray zone without nanostructure. The size of PM-W sample is $10 \times 10 \times 0.1$ mm³.

Figure 14 shows microscopic views for the above sample, where (a) and (c) show the cross-section, and (b) and (d) are grazing views for these areas. Now, the thickness of carbon layer decreased from about 500 nm down to 140 nm probably due to sputtering by helium ions. We found that the carbon thin layer protect against the formation of nanostructure. Such an inhibition of fuzz structure formation was originally reported by PISCES group ²²⁾. Here a more visual way has been demonstrated.



Fig. 14 FE-SEM photos for two areas seen in Fig.13. Here (a) and (b) show the top and grazing views of black zone, while (c) and (d) do those at gray zone.

4. Summary and Conclusion

Precise estimation for the radiation capability of nanostructured W has been obtained in terms of total emissivity (TE) by using electron beam calibration system in vacuum. The black nanostructured W surface was found to play as an almost complete black-body. The questions related to the fixed biasing method for obtaining the TE are discussed in terms of ion energy reflection and a cooling associated by SEE. It is recognized that the power transmission factor through the plasma sheath is very important, especially for the surface with a change in surface morphology.

The unfavorable property of such He-defected W are discussed from the points of view of dust formation. Some recovery process to obtain an original flat surface are represented focusing on the ITER grade PM-W although the tiny bubbles remain underneath the surface, and thin carbon coating with the thickness of a few hundreds nanometer is demonstrated to represent a kind of protective layer against the formation of He defects. In the case of ITER, beryllium would take a place of carbon.

Acknowledgements

The research work was supported by Grant-in-aid for Scientific Research (B) 20360414, Grant-in-Aid for Challenging Exploratory Research 23656578, and Grant-in-aid for Scientific Research (A) 2246120 from JSPS, and also by The Science Research Promotion Fund from the Promotion and Mutual Aid Corporation for Private School of Japan. The authors would like to thank H. Iwata of AIT for his help on FE-SEM manipulation and Dr. S. Kajita of Nagoya University for his valuable discussions.

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(受理 平成25年3月19日)